OptumG3

Verification of Mohr-Coulomb model in different soil tests



Soil tests

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9 Aug 2019

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1 Introduction

1.1 Failure criterion

The Mohr-Coulomb failure criterion is given by

$$F = |\sigma_1 - \sigma_3| + (\sigma_1 + \sigma_3)\sin\phi - 2c\cos\phi = 0 \tag{1.1}$$

where c is the cohesion and ϕ is the friction angle. The principal stresses (positive in tension) are ordered as:

$$\sigma_1 \le \sigma_2 \le \sigma_3 \tag{1.2}$$

1.2 Elastic law

The Mohr-Coulomb model uses Hooke's law which is given in terms of principal stresses and strains by

$$\begin{pmatrix}
\varepsilon_1 \\
\varepsilon_2 \\
\varepsilon_3
\end{pmatrix} = \frac{1}{E} \begin{bmatrix}
1 & -\nu & -\nu \\
-\nu & 1 & -\nu \\
-\nu & -\nu & 1
\end{bmatrix} \begin{pmatrix}
\sigma_1 \\
\sigma_2 \\
\sigma_3
\end{pmatrix}$$
(1.3)

where E is Young's modulus and ν is Poisson's ratio.

1.3 Biaxial test

In biaxial compression, failure occurs when

$$\sigma_{1,f} = \sigma_3 \frac{1 + \sin\phi}{1 - \sin\phi} - 2c \frac{\cos\phi}{1 - \sin\phi} \tag{1.4}$$

1.4 Triaxial tests

In triaxial compression, failure occurs when

$$\sigma_{1,f} = \sigma_3 \frac{1 + \sin\phi}{1 - \sin\phi} - 2c \frac{\cos\phi}{1 - \sin\phi} \tag{1.5}$$

while, in extension, failure occurs when

$$\sigma_{3,f} = \sigma_1 \frac{1 - \sin \phi}{1 + \sin \phi} + 2c \frac{\cos \phi}{1 + \sin \phi} \tag{1.6}$$

In triaxial compression with $\,\sigma_1 < \sigma_2 = \sigma_3$, the strains below failure are given by

$$\varepsilon_1 = \frac{1}{E} \ \sigma_1 - 2\nu\sigma_3 \ , \ \varepsilon_2 = \varepsilon_3 = \frac{1}{E} \ (1 - \nu)\sigma_3 - \nu\sigma_1$$
 (1.7)

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Biaxial test 2

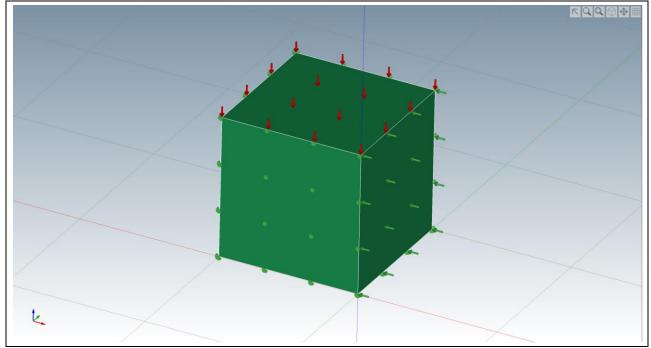


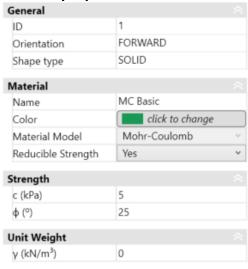
Figure 1: Biaxial test

Benchmark 260.88 **Results** 260.00 **Discrepancy** 0.00%

General description:

Cubic 5x5m specimen. Selected sides normally supported to reproduce plane strain conditions. A fixed load of -100 kPa is applied along with a multiplier load of -1kPa. Limit analysis is then used to determine the collapse multiplier.

Material properties:



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3 Triaxial compression test

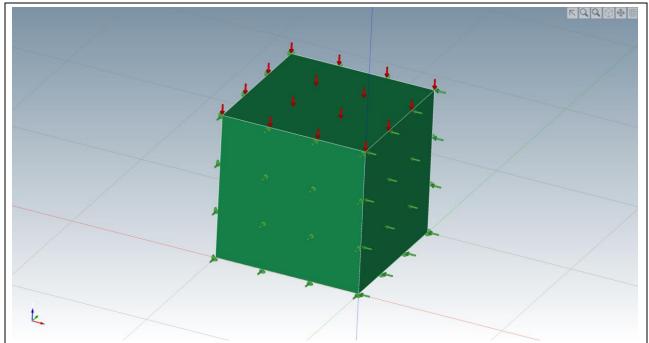


Figure 2: Triaxial compression test

 Benchmark
 260.088

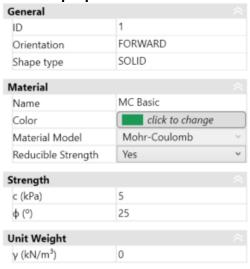
 Result
 260.088

 Discrepancy
 0.00%

General description:

Cubic 5x5m specimen. Selected sides normally supported to reproduce triaxial conditions. Fixed load of -100 kPa are applied along with a multiplier load of -1kPa. Limit analysis is then used to determine the collapse multiplier.

Material properties:



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4 Triaxial extension test

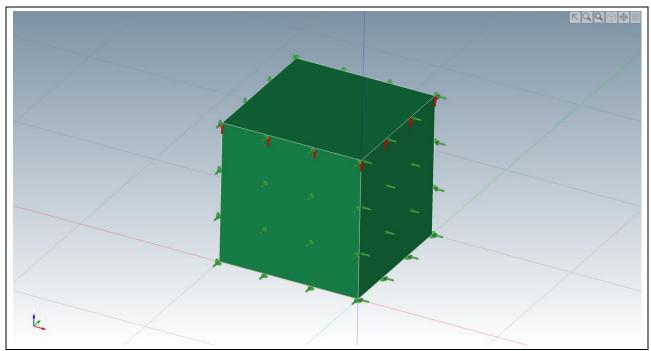


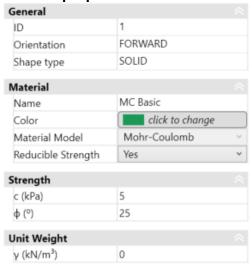
Figure 3: Triaxial extension test

Benchmark -34.215 Result -32.215 Discrepancy 0.00%

General description:

Cubic 5x5m specimen. Selected sides normally supported to reproduce triaxial conditions. Fixed load of -100 kPa are applied along with a multiplier load of 1kPa. Limit analysis is then used to determine the collapse multiplier.

Material properties:



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5 Displacements

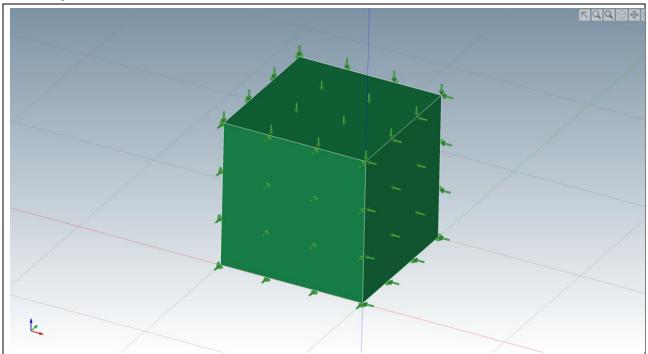


Figure 4: Triaxial compression test for elastic analysis

Results:

	Result	Benchmark	Discrepancy (%)
$arepsilon_1$	-1.5	-1.5	0.00%
$arepsilon_2$	-0.25	-0.25	0.00%
ε_3	-0.25	-0.25	0.00%

General description:

Cubic 5x5m specimen. Selected sides normally supported to reproduce triaxial conditions. Fixed load of -100 kPa are applied horizontally along with a fixed load of -200 vertically. Elastic analysis is then used to determine the displacements.

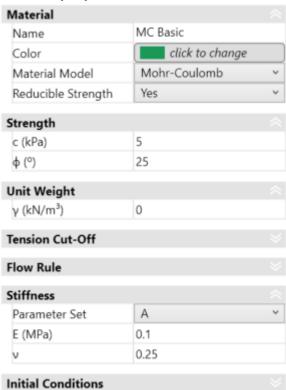
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Material properties:



Stage settings:

